Fabrication and Characterization of Porous Silica Monolith by Sintering Silica Nanoparticles

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Abstract

This paper aims to fabricate over centimeter size of porous silica monolith having meso-pores with large surface area. A precursor of porous silica monolith was obtained by sintering a monolithic SiO₂-poly (vinyl alcohol) (PVA) nanocomposite at 600°C - 1100°C. The sintering behavior was examined by means of Raman spectroscopy and a porosimetry. The PVA of the SiO₂-PVA nanocomposite was combusted below 600°C, subsequently the silica nanoparticles of the nanocomposite were sintered above 900°C. The Raman spectroscopy suggested that amorphous structure of the porous silica monolith obtained above 1000°C was similar to that of a silica glass. The BET surface area and pore radius of the porous silica monolith decreased with increasing sintering temperature. These values were tailored in the range of ca. 0 - 291 m²·g⁻¹ and 5 - 25 nm, respectively, by controlling the sintering temperature and time. The fabricated porous-silica monolith was translucent or opaque porous-silica depending on the pore size.

Keywords

Porous Silica, Monolith, Silica Nanoparticles, Silica Glass, PVA, Sintering

1. Introduction

A porous silica monolith of over centimeter size with a large surface area has been growing research interest for application to various industrial fields such as a catalysis, thermal insulation, adsorption, and separation. Sol-gel processes have been widely adapted for fabricating a porous silica monolith to control a pore size [1]-[8]. On the other hand, a particulate sol-gel process, which uses silica nanoparticles as a starting material, is also attractive alternative to fabricate a
large porous silica monolith. For the past decades, the particulate sol-gel process has been developed for fabricating a porous silica precursor for a monolithic silica glass [2]. In the particulate sol-gel process, the porous silica precursor of porous silica monolith was prepared via gelation of a silica suspension and gel drying. It has been reported to fabricate over centimeter size of the porous silica precursor, as well as a silica glass monolith by sintering, with a shape of rods [9] [10] [11] [12] [13], tubes [14] [15] [16] [17] [18], rings [19], and plates [20]. However, some cracks often arise on a porous silica monolith during the gel drying step because a capillary force generates in the pores. This critical issue makes it difficult to fabricate large size and complex shape of porous silica monolith. In order to overcome the crack generation, important developments for the particulate sol-gel process have been widely studied. For instance, to suppress the crack generation during gel drying, many research groups have used dozens nanometer size of silica particles with adding some chemical additive [9]-[20].

Alternatively, we newly developed a particulate sol-gel process using single nanometer size of fumed silica particles, instead of several dozen nanometer sizes, in addition to use of poly(vinyl) alcohol (PVA) to avoid the crack generations during gel drying [21]. This process allows fabricating a porous SiO₂-PVA nanocomposite monolith which can be used as a silica glass precursor. The monolithic SiO₂-PVA nanocomposite, without any crack generation during drying of a gel, has relatively large surface area which can be controlled in the range of 100 - 300 m²·g⁻¹ [22]. In this study, we further developed the process to fabricate a porous silica monolith via sintering process by using the monolithic SiO₂-PVA nanocomposite as the precursor. The surface area and pore size of the obtained porous silica monolith were tailored by the sintering temperature and time.

2. Experimental

2.1. Fabrication of Porous Silica Monolith

An SiO₂-PVA nanocomposite, which is the precursor of a porous silica monolith, was prepared by using fumed silica nanoparticles (Aerosil 300, BET surface area of 300 m²·g⁻¹ according to the supplier, Nippon Aerosil, Japan) and PVA (polymerization degree of 1500 - 1800, Wako pure chemical Industries, Japan) as starting materials by a following procedure [21]. Fumed silica was added distilled water adjusted at pH 3 followed by dispersing by means of an ultra-sonication for 1 h to obtain 8 wt% of a silica suspension. Meanwhile, PVA was dissolved into distilled water and stirred using a magnetic stirrer at a speed of 800 rpm to prepare 8 wt% of a PVA solution. Then, the obtained silica suspension and PVA solution were mixed for 12 h to obtain 80SiO₂-20PVA (wt%) suspension. The resulting SiO₂-PVA suspension was cast into a Teflon container and dried at 30°C under atmospheric pressure in an oven. A gelation of the suspension was taken place gradually and then a monolithic SiO₂-PVA nanocomposite was formed.

A monolithic porous silica monolith was fabricated by calcining the SiO₂-PVA nanocomposite at 600°C for 3 h in air to combustion of the PVA, followed by
sintered at 600°C - 1100°C for 5, 10, 20, 30 min, or 1 h, respectively, in air.

2.2. Characterization of Porous Silica Monolith

BET surface area and pore size distribution of the porous silica monolith were determined by means of a porosimeter (BELSORP-mini, Bel Japan Inc., Japan) via Brunauer-Emmett-Teller (BET) method and Barrett-Joyner-Halenda (BJH) method. Structural change in the porous silica monolith by the sintering was examined by means of a Raman spectrometer (STR-HTUV, Seki Technotron Co.) equipped with a He-Cd laser. Optical transmittances of the porous silica monolith were measured by means of a spectrophotometer (U-3500, Hitachi High-Technologies Co., Japan).

3. Results and Discussion

3.1. Sintering Behavior of Silica Nanoparticles

Figure 1 shows pore size distribution of the SiO$_2$-PVA nanocomposite. It is clearly seen that the SiO$_2$-PVA nanocomposite had mesopores with radius below 20 nm and BET surface area of 141 m$^2$·g$^{-1}$. This SiO$_2$-PVA nanocomposite was used as a precursor for a porous silica monolith. The SiO$_2$-PVA nanocomposite precursor was sintered at given temperature in the range of 600°C - 1100°C to fabricate a porous silica monolith. Figure 2 denotes dependence of BET surface area on sintering temperature for the sintered samples. BET surface area for the sample sintered at 600°C was 291 m$^2$·g$^{-1}$. This value is larger than that of the SiO$_2$-PVA nanocomposite precursor and comparable to that of the as-received fumed silica particles. This result indicated that the PVA in the SiO$_2$-PVA nanocomposite was just combusted at the temperature and sintering of the silica nanoparticles did not occur. As increasing sintering temperature up to 900°C, BET surface area of the sample decreased with increasing treatment temperature. Over 900°C, BET surface area of the sample abruptly decreased with increasing sintering temperature. This fact suggested that the sintering of silica
Figure 2. Dependence of sintering temperature on BET surface area for the porous silica monolith obtained by calcining the SiO$_2$-PVA nanocomposite at 600°C for 3 h in air, followed by sintering at each temperature for 1 h in air.

Figure 3. Pore size distributions of porous silica monolith obtained by calcining the SiO$_2$-PVA nanocomposite at 600°C for 3 h in air, followed by sintering at each temperature for 1 h in air.

nanoparticles would occur above 900°C. At 1100°C, BET surface area reached to zero. This result indicates that sintering of the silica nanoparticles was accomplished at 1100°C and dense (non-porous) body was formed. Figure 3 shows dependence of the sintering temperature on pore size distributions of the sintered silica samples. It is clearly seen that the sintered silica samples had broad peaks with the pore radius below 25 nm. For the sample sintered at 600°C, the peak center of pore size distribution is located at ~15 nm. As increasing sintering temperature, the peak was shifted to smaller side and its peak intensity became small. For the sample obtained at 1100°C, no pores exist in the examined range.

Sintering behavior of the silica nanoparticles of the SiO$_2$-PVA nanocomposite was elucidated in terms of change in amorphous structure by using the Raman spectroscopy. Figure 4 depicts Raman spectra of the sintered silica samples. Raman spectrum for a commercial silica glass was also given in the figure to
Figure 4. Raman spectra of (a) SiO$_2$-PVA nanocomposite, and the sintered samples at (b) 600˚C, (c) 800˚C, (d) 900˚C, (e) 1000˚C, (f) 1100˚C for 1 h in air, and (g) a commercial silica glass.

Figure 5 depicts relative intensities for D1 and D2 bonds of each sample. For the spectrum of SiO$_2$-PVA nanocomposite, the intensities for D1 and D2 bands relatively larger than those of the commercial silica glass. As increasing sintering temperature, intensities for D1 and D2 bands decreased. As a result, the intensities for the sample sintered at 1100˚C became to be comparable to those of the commercial silica glass. These changes in the intensities would involve structural change in silica members rings. Amorphous silica contains silica members rings such as four-membered (D1) and three-membered (D2) silica rings, and larger members silica rings. In an industry, the fumed silica nanoparticle, used in this study as the starting material, is produced by hydrothermal reaction of SiCl$_4$ in oxyhydrogen flame at high temperature. The production process for the fumed silica nanoparticles gives characteristic surface properties such as large surface area and structural defects such as four-membered (D1) and three-membered (D2) silica rings. These four-membered and three-membered silica rings are considered to be less stable than the other members rings such as six-membered rings [27]. Thus,
such small membered rings would be transformed to the other stable structure during sintering. Figure 4 and Figure 5 suggested that the structural change of the amorphous silica was observed in the sample sintered above 900°C. Consequently, the amorphous structure for the sample sintered at 1100°C is comparable to that of the commercial silica glass. From these results, it is considered that sintering of silica nanoparticles occurs above 900°C, associated with change in the amorphous structure between transformed from three- and four-membered silica rings to the other membered rings.

3.2. Characterization of Porous Silica Monolith Obtained by Sintering

Porous structure of sintered silica monolith is also controlled by sintering time, as well as sintering temperature. Figure 6 shows variation of BET surface areas by change in the treatment time at 1100°C in air. The BET surface area of the sample decreased with increasing time. As shown in Figure 7, the pore size distribution for the sample shifted to lower side with increasing sintering time. These results indicated that the porous structure was tailored with BET surface area.
Figure 6. BET surface areas of porous silica monolith obtained by calcining the SiO$_2$-PVA nanocomposite at 600°C for 3 h in air, followed by sintering at 1100°C for given time in air.

Figure 7. Pore size distributions of the porous silica monolith obtained by calcining the SiO$_2$-PVA nanocomposite at 600°C for 3 h in air, followed by sintering at 1100°C for given temperature in air.

area in the range of ca. 0 - 300 m$^2$ g$^{-1}$ and pore size distribution in ca. 5 - 30 nm, respectively.

The sintering time affects not only on the porous structure but also an optical transmittance in UV-Vis and near-infrared regions. Figure 8 shows optical transmittance in UV-Vis and near-infrared regions for the sintered samples. For the sample (a) obtained by sintering at 1100°C for 5 min, whose BET surface area was 146 m$^2$ g$^{-1}$, the spectrum indicated opaque in the examined range. In contrast, for the sample; (b) obtained by sintering at 1100°C for 30 min, whose BET surface area was 20 m$^2$ g$^{-1}$, the sample was translucent. In order to clarify the relation between the morphology and the optical transmittance, we observed the microstructure of the sintered sample by using FE-SEM. Figure 9 shows FE-SEM images for these samples. For the opaque sample, the silica grains with several hundred nanometer and inter-particle pores were clearly observed. For
Figure 8. Optical transmission spectra of the porous silica monolith obtained by sintering at 1100°C for (a) 5 min, (b) 30 min.

Figure 9. FE-SEM images of the silica monolith obtained by sintering at 1100°C for (a) 5 min, (b) 30 min.

Figure 10. Photograph of the porous silica monolith obtained by sintering at 1100°C for 5 min.

The translucent sample, meanwhile, the grain size became large and inter-particle pore size was reduced. It is considered that decreasing of inter-particle pore size reduced a light scattering at the particle interface. Therefore, transmittance of the porous silica increases with decreasing BET surface areas.

Figure 10 shows the porous silica monolith fabricated by using the present method. We obtained the disc shape with 63 mm diameter and 7 mm thickness. No crack was observed by the naked eye. The BET surface area for the porous silica monolith (e.g. 146 m²·g⁻¹) is much larger than that of silica monolith obtained by a conventional colloidal gel process (e.g. less than 50 m²·g⁻¹) [2].
Therefore, the present method is attractive alternative to fabricate porous silica monolith with over centimeter size possessing mesopores.

4. Conclusion

A porous silica monolith was fabricated by sintering the monolithic SiO$_2$-PVA nanocomposite containing silica nanoparticles. Sintering of the silica nanoparticles occurred above 900˚C with change in the amorphous silica structure. The BET surface area and pore radius can be tailored in the range of 0 - 300 m$^2$·g$^{-1}$ and 5 - 25 nm, respectively, by optimization of sintering temperature and time. We obtained successfully large size of the porous monolith of the disc shape with large surface area. In future, it is expected that complex shape (e.g. tube, honeycomb structure) products are fabricated by the present method.

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