The Study on New Solid-State Breaker and Its Over-voltage Suppression Technique

Longji Zhu, Yan Zheng
Anhui University of Science and Technology, Huainan, Anhui, China
Email: ljzhu@aust.edu.cn
Received January, 2013

ABSTRACT
A design scheme of the intelligent SSB (Solid State Breaker) based on the IGCT (Integrated Gate Commutated Thyristor) is presented. The topology of switch module and the structure of the SSB are proposed. Firstly, to the IGCT’s over-voltage sensitivity problem, a new technique of reducing the over-voltage is introduced, which releases the elect romantics energy of faulty line by a capacitive current branch to reduce the amplitude of over-voltage. Secondly, the principle of over-voltage suppression with current release branch is analyzed, and the overall control scheme of solid-state breaker is put forward. Finally, the simulation results also demonstrate its obvious effectiveness in over-voltage suppression after adding a current release branch into the SSB.

Keywords: Solid-state Breaker; IGCT; Over-voltage Suppression; Current Release Circuit

1. Introduction
With the construction of the distributed power grid of China, the requirement of the performance for the transmission equipments in power system is getting higher. How to improve the stability and reliability of power transmission equipments becomes the development direction of the electric power industry. The Breaker is important equipment in transmission lines, and it’s performance directly impacts the normal operation of the power grid. A large number of mechanical breakers are used in the transmission system, although it has the advantages of stable conduction, strong load ability, but there are not flexible, real-time, continuous and fast actions, easy to make the expansion of circuit fault and other shortcomings. When the load current is disconnected, the breaker contact is easy ablated by the electric arc, cutting time delay, so it is difficult to meet requirements of some electricity users for fast reaction speed of the fault current, there is noise in the operation process, the mechanical and electrical life limited[2,5]. Solid state circuit breaker can be used as the key equipment of the flexible AC transmission system, which can realize fast, flexible, accurate control of the power system parameters and grid structure. The SSB based on power switch devices, because of its outstanding performance of the switch current caused widespread concern, since the advent of them. According to related literatures, the 15 kV/600A high-voltage solid-state breaker is manufactured in the Malveren City High Power Electronic Devices Factory, which can finish the cutting current in 4 milliseconds. The 13 kV/675A high-voltage solid-state breaker is developed in Westinghouse Company. The solid-state breaker for the 13kV power distribution also is developed in United Kingdom[7]. The IGCT (Integrated Gate Commutated Thyristor) with low on-stage voltage is used in this paper, and this solid-state high-voltage breaker applies to the 10 kV grid voltage level. The breaker’s breaking time up to microseconds in short circuit situation. It also can limit the fault current and improve the stability of the system. And it is totally sealed and non-contacts structure, long service life, do not switch the number of restrictions, reduce the failure rate. The over-voltage mechanism of the SSB is analyzed, the inhibition of its Over-voltage method is adopted to increase the resistance and capacitance branches can make switching over-voltage suppression in the allowed range.

2. The New SSB
The switch module of the new SSB, which is based on the IGCT, applied to the 10 kV grid voltage level. The IGCT is a new type of power electronic device, and it can be used as the first choice of the new solid-state breaker because its high-voltage, big-current, smaller switching losses, and fast switching speed, etc... The technology parameters of IGCT manufactured by ABB Company are shown in Table 1. In order to reduce the number of devices and improve the reliability of the system, two 4.5 kV IGCTs are in series to 9 kV switch module.
Considering the fluctuations in grid peak voltage, the breaker nominal voltage should designed at least up to 13kV, coupled with one device redundancy, so the SSB are composed in series by two 9 kV switch module. The switch module topology is shown in Figure 1; composed by two inverse parallel branches of two IGCT connected in series, and respectively conducted the positive and negative current. Each IGCT series branch connected additional 9 kV rectifier diode to protect the IGCT. Each device is connected by parallel buffer circuit of the $\frac{dv}{dt}$, voltage-sharing resistors and thyrite arrester. Because of the low over-current capacity, the SSB need to increase the $\frac{di}{dt}$ snubbed circuit when the connected in series switch module.

The control strategy of the SSB includes two parts: normal operation and fault handling. In normal operation, the SSB takes soften switching control strategy, i.e. the switch is off when the current is zero, and is on when the voltage is zero[6]. When the system is in failure, the breaker should immediately disconnect the faulted line, and protect the sensitive loads work in normal. When the load side is in short circuit fault, the first step is to turn off switching devices rapidly, if the failure was excluded in a half cycle, then to turn on the switching devices; Otherwise, the parallel current-limiting switch is to turn on, and the aim is to make the fault current limiters in maximum of 15 working cycles in order to protect the load side equipment [1].

The SSB has the characteristic of fast action, which is conducive to rapid fault isolation, in order to protect the electrical equipment and to prevent the failure to expand. But because the SSB’s breaking speed is too fast, shut-off the current and other reasons, the device need to withstand the impact of very high over-voltage. Over-voltage protections in the SSB mainly rely on two ways: resistance and capacitive snubbed circuit and zinc oxide surge arrester [4]. The over-voltage buffer circuit is shown in Figure 1, the capacitor $C_s$ is generally about 2μF, if the $R_s$ is too small, the over-voltage caused by breaking the short-circuit current will increases the buffer capacitor inrush current; if $R_s$ is too large, the response speed of the buffer circuit reduces. So it can not achieve the desired effect of the over-voltage. The above two ways are the passive protections of over-voltage, can not fundamentally eliminate the over-voltage generated [3,7]. Therefore, how to limit the amplitude of the over-voltage fault isolation process is a high level of research and application value.

Due to the fast shutdown of the IGCT, if the influence of the IGCT’s tail current and the RC snubbed circuit are ignored, the SSB can be treated as an ideal switch. When the SSB receives a shutdown signal, it will instantly disconnect the short-circuit current. The energy stored in the stray inductance and the distributed capacitance in the circuit will produce electromagnetic oscillations. Its equivalent circuit is shown in Figure 2.

Supposing $E$ as the electromagnetic energy stored in the line, it can be expressed as equation (1):

$$E = \frac{1}{2} C_s \left( \frac{dv}{dt} \right)^2 + \frac{1}{2} R_s \left( \frac{di}{dt} \right)^2$$

Table 1. Mostly technique parameter of IGCT.

<table>
<thead>
<tr>
<th>Instantaneous switching frequency</th>
<th>20KHz</th>
</tr>
</thead>
<tbody>
<tr>
<td>Switching off time</td>
<td>1μs</td>
</tr>
<tr>
<td>$\frac{dv}{dt}$</td>
<td>10~20KV/μs</td>
</tr>
<tr>
<td>$\frac{di}{dt}$</td>
<td>4KA/μs</td>
</tr>
<tr>
<td>AC blocking voltage</td>
<td>6.5KV</td>
</tr>
<tr>
<td>DC blocking voltage</td>
<td>4.5 KV</td>
</tr>
</tbody>
</table>
Therefore, increasing the capacitance to ground in the SSB load side can reduce the transient over-voltage amplitude. The voltage of the SSB withstands \( u_s(t) \) is:

\[
u_s(t) = u_e(t) - u_C(t)
\]

(2)

According to the KVL equation, the maximum over-voltage of the SSB can be obtained as followed:

\[
u_s(t) = u_e(t) + 0.5 \frac{I_{GCT}^2}{C} e^{-R/L \sigma}
\]

(3)

\[
\sigma = \sqrt{\left(\frac{R}{2L}\right)^2 - \frac{1}{LC}}
\]

The \( u_e(t) \) is the instantaneous voltage in power supply side; \( u_C(t) \) is the instantaneous voltage of the load side. The \( C \) is the distributed capacitance to ground. The \( R \) and \( L \) are the resistance and inductance of the load side respectively. According to equation (3), increasing the capacitance \( C \), the amplitude of over-voltage can be effectively weakened, when the SBB cut off the line. Therefore, a resistance and capacitor branch is connected in parallel. The resistance-capacitor branch, which can increase the capacitor \( C \) to ground, and to reduce the voltage amplitude, is controlled by the GTO, and the GTO will work before the SSB works. Its equivalent circuit is shown in Figure 3[3].

In order to verify the inhibition effect of the over-voltage after increasing the resistance and capacitance branch, the simulation of the SSB’s capacity of breaking the single-phase short circuit fault is analyzed by the Simulink and PLES simulation software. The power supply phase voltage is 5.7 kV (line voltage is 10 kV), before the short-circuit fault occurs, the equivalent load resistance and inductance are 120 Ω and 8mH. The distributed parameters of fault line: nominal cross-section is 120 mm²; Current carrying capacity is 290 A; Resistance is 0.153 Ω/km; Inductance is 0.356mH/km; Capacitance is 0.29 μF/km. The breaking voltage waveform before and after the increased resistive and capacitive branch is shown in Figure 4, the voltage amplitude is the unit value (pu units). The breaking over-voltage of the SSB without the resistance-capacitance branch is about 1.8 pu; and the breaking over-voltage with the resistance and capacitance branch decreased to 1.20 pu.

4. Conclusions

New solid-state breaker using IGCT excellent turn-off
capability and fast turn-off characteristic can isolate rapidly the circuit fault and prevent the expansion of the fault. But due to the solid state circuit breaker is too fast, need to withstand over-voltage impact is very high, the need to increase the resistance-capacitance freewheeling branch. Through the simulation test of 10 kV voltage, the SSB without the freewheeling branch’s breaking over-voltage is up to 1.8 pu, and after increasing the freewheeling branch, the breaking over-voltage is reduced to 1.2 pu. Therefore, the freewheeling branch support the energy releasing channel, which not only significantly suppress the breaking over-voltage, also clear the residual charge on the line, eliminating the hidden danger of over-voltage when the SSB closing.

REFERENCES


