Controlled-Release Analysis of Potassium Permanganate Using PMMA Matrix

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Received 22 August 2014; revised 13 October 2014; accepted 22 October 2014

Abstract
Excess amount of potassium permanganate has often been used in-situ for chemical oxidation of contaminated sites. The consequences are not limited to secondary contamination and cost but also inefficient remediation. Encapsulation of permanganate using PMMA enables controlled dissolution of the oxidant and aids long-term processes. This paper focuses on the oxidant release efficiency from polymer matrix and analysis of data using existing models for glassy polymers. The efficiency profile obtained using mass ratios of 2:1, 4:1, and 8:1 of PMMA to KMnO₄ showed a decrease in the extent of release with increasing mass ratio with 79%, 55.35% and 33.59% respectively. Patches were noticed on the surfaces of PMMA after the release of KMnO₄, these were attributed to crevices created by the non-fickian diffusion of the oxidant.

Keywords
PMMA, Controlled-Release, Permanganate, Analysis, Encapsulation

1. Introduction
In situ chemical oxidation (ISCO) has been successfully used to degrade chlorinated hydrocarbons for decades [1] [2]. One popular oxidant in ISCO application is potassium permanganate, KMnO₄ possibly due to its high oxidation potential across the pH [3]. This oxidant is highly soluble in aqueous media but largely insoluble in non-polar solvents (e.g. TCE contaminated zone). Thus, as a strong and reactive oxidant, KMnO₄ would oxidize any reductive material dissolved in an aqueous medium. The amount of KMnO₄ therefore available to oxidize target contaminant is likely consumed by dissolved organic constituent, thereby decreasing the oxidation efficiency. More KMnO₄ than necessary is therefore used for complete degradation of the target compound [4].
Therefore, the availability of KMnO₄ in aqueous phase can be controlled by slowing down its dissolution rate, thereby enabling oxidant persistence.

Controlled-release technology has widely been used in biopolymer engineering in drug delivery applications [5]-[7]. This enabled the control of dissolution rate and delivery to targeted parts due to preferential interaction. Similarly, the controlled-release application of KMnO₄ in soil and water treatment should not only control the rate of oxidant dissolution but also improve effective interaction with target contaminant. This is achieved by encapsulating the water soluble KMnO₄ with a responsive polymer that is not soluble in water [8]. Thus, the outer surface barrier prevents direct contact between the oxidant and the aqueous medium. Poly(methyl methacrylate) (PMMA) is hydrophobic and responsive to chlorinated hydrocarbons’ solvent environment. However, before this study PMMA has not been investigated for oxidant encapsulation.

Poly(methyl methacrylate) (PMMA) is a synthetic resin produced from the polymerization of methyl methacrylate, a transparent rigid plastic and often referred to as organic glass. PMMA, an ester of methacrylic acid (CH₂ = C[CH₃]CO₂H), belongs to the important acrylic family of resins. In modern production it is obtained principally from propylene. Methyl methacrylate, (CH₂ = C[CH₃]CO₂H₃) in bulk liquid form or suspended as fine droplets in water, is polymerized (its molecules linked together in large numbers) under the influence of free-radical initiators to form solid PMMA. The structure of the polymer repeating unit is presented in Figure 1.

More studies would be required to understand the release mechanism of KMnO₄ from PMMA encapsulation. However, this study centers on the oxidant release efficiency of PMMA in aqueous system and the matrix surface analysis.

2. Materials and Methods

2.1. Reagents

Poly (methymetacrylate) (PMMA) bead particles was ordered from Acros Organics; Sodium Borate purchased from Mallinckrodt, inc; Acetone (100%) was purchased from Acros Organics; Trichloroethylene, 100% (American Chemical Society, ACS grade), potassium permanganate (oxidant), sodium thiosulfate (used to quench reaction) and HPLC grade hexane (liquid-liquid extraction) were all purchased from Fisher Scientific. De-ionized water was used for all experiments.

2.2. Encapsulation Procedure

KMnO₄ (oxidant) was encapsulated in PMMA matrix by adapting and modifying the molten suspension and cooling method at room temperature [8]. A predetermined amount (e.g. 2 g) of PMMA was measured into a 100 ml beaker and 3 ml acetone is added. The PMMA whose melting point is very high melts at room temperature under the influence of acetone. The molten PMMA is placed on a stirrer and mixed thoroughly using a glass magnetic arrow. Borax (Sodium Borate) was added to initiate cross-link of the molten PMMA. Under continuous mixing, particles of KMnO₄ were added as required to produce 1:2, 1:4 and 1:8 of KMnO₄ of PMMA ratio. After mixing for 10 mins to assume uniform particle dispersion, the molten mixture was allowed to solidify under room temperature by volatilizing acetone. Solidified particles/granules of encapsulated KMnO₄ were reduced using laboratory mill. Sieved sizes were used as needed for the release experiments. The flow diagram (see Figure 2) depicts the encapsulation process.
2.3. Release Experiments

Encapsulated KMnO₄ for control release experiment were used in the ratios of 1:2, 1:4, and 1:8 of the KMnO₄/PMMA matrix. A calculated amount of the encapsulated KMnO₄ ranging from 300 to 900 mg containing equivalent amount of the oxidant were used. At ambient condition, the modified oxidant was introduced into a 1-L Milli-Q de-ionized water with continuous mechanical stirring to enable uniform solution. At specific time intervals, aliquots of the solution were taken, centrifuged and analyzed for KMnO₄ using Cary UV Spectrophotometer at 525 nm wavelength. Release profiles were developed for the mass of KMnO₄ released with time. The amount of KMnO₄ initially contained in the PMMA matrix was calculated as below:

\[ X = P + K \] (1)

But ratio (r) of PMMA/KMnO₄ can be represented as

\[ r = \frac{P}{K} \text{ or } P = r^*K \] (2)

where \( X \) = weighed total mass of PMMA and KMnO₄ in the encapsulated form, \( K \) = Mass of unmodified KMnO₄ particles per mass of encapsulated matrix, \( P \) = mass of PMMA bead particles per mass of encapsulated matrix and \( r \) = ratio of PMMA to KMnO₄ in a specific matrix.

3. Results and Discussion

3.1. Release Experiment for Encapsulated KMnO₄ in Water

The release profile for KMnO₄ in Water was studied with mass to mass ratios of 1:2, 1:4, and 1:8 of KMnO₄ to PMMA particles respectively. The results indicate that the release efficiency is inversely proportional to the mass ratio of KMnO₄ to PMMA particles. There was decrease in release with increasing mass ratio (see Figure 3). At a 10-hour time period, 79%, 55.35% and 33.59% of KMnO₄ has been released from 1:2, 1:4, and 1:8 encapsulated matrix respectively. PMMA is not soluble in water hence initial release near time \( t = 0 \) is most likely dissolution of KMnO₄ integrated on the surface of encapsulated matrix. Therefore the lowest release rate associated with 1:8 mass ratio was due to the thickness of the PMMA layer in the encapsulated matrix.

3.2. Analysis of Release

The release of KMnO₄ from the surface of the PMMA matrix left some patches and holes under SEM imaging (see Figure 4(b)). The structural changes on glassy polymer surfaces have been attributed to possible effects of STRESS and strains on surface as the material swells [9]. This is suggested to be as a result of response to any of the following: effects of temperature change, effects of activity differences, and effects of prehistory and sample dimensions [10]-[12]. The release has therefore been modeled as non-fickian where diffusion and dissolution depends on stress on the matrix and not on concentration gradient.
Figure 3. Release profile KMnO₄ from PMMA encapsulated KMnO₄.

Figure 4. (a) SEM image of the surface of PMMA encapsulated KMnO₄ before release experiment; (b) SEM image of the surface of PMMA encapsulated KMnO₄ after release experiment.
The initial swelling/dissolution from the matrix surface leaves patches and holes on the matrix. These holes allow the aqueous phase to diffuse into the inner opening of the PMMA matrix contacting more KMnO₄ [8]. Thus the release mechanism for glassy polymers (such as polystyrene, PMMA) had previously been modeled as below [10]:

\[ S_e = at^n \] (3)

where \( S_e \) is the percent release of the oxidant, \( t \) is the time period for specific \( S_e \), constant \( a \) is the characteristic property of the encapsulated matrix and exponent \( n \) varies with parameters of structural changes. Figure 4(a) and Figure 4(b) compares respectively the SEM images of encapsulated matrix before and after oxidant release.

Equation (3) can be represented in the logarithmic form as shown in Equation (4). A plot of \( \log S_e \) against \( \log t \), give the slope as \( n \) while \( k \) is obtained from the intercept. Thus, the time required for every percent release can be obtained from the model.

\[ \log S_e = \log a \ n \log t \] (4)

For the mass ratio 1:8, a plot of \( \log S_e \) against \( \log t \) gives the value \( n = 0.2611 \) and \( k = 6.75 \times 10^{-2} \). Therefore the model can be represented as

\[ t_{S_e} = \left[ \frac{S_e}{6.75*10^{-2}} \right]^{1/0.2611} \] (5)

### 4. Conclusion and Recommendation

PMMA was effective in controlling the instant dissolution of KMnO₄ in aqueous media. The release rate is very low and depends on the thickness of the PMMA layer on oxidant surface. Results showed that the encapsulation of KMnO₄ by PMMA using the modified molten suspension technique controlled the rate of dissolution of KMnO₄. The interaction mechanism between PMMA and KMnO₄ during encapsulation is not discussed in this paper. The analysis of release data attributed to crevices obtained on the surfaces of PMMA is according to models for other glassy polymers. This study provides insight into the application of PMMA in oxidant release and persistence in long-term leaching organic contamination.

### References


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