Methods to Minimize Optical Noise That Degrade Fluorescence Efficiency of Optical Probe for Near-Infrared Tracking in Surgical Environment

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Abstract

In the medical field, there are growing interests in applied research such as in vivo fluorescence monitoring because of excellent body transmission characteristic of the near-infrared light. However, optical noise by excitation light and illumination equipment for medical applications such as interior light, surgical light decrease efficiency of the fluorescent signal when observers such as surgeons confirm fluorescence signals in medical field. To solve these problems in medical field, we have analyzed external noise factors by effect on image realization, quantification of optical noise generation by external factors, and have suggested methods of minimize the optical noise in this paper. In case of fluorescence imaging in the operating room, it has been confirmed that fluorescent excitation light, interior light and surgical light are factors to generate optical noise. To acquire near-infrared fluorescence images and to compare fluorescence contrast under conditions of darkroom, interior light and surgical light, light emitting diodes (LEDs) sources that have peak wavelength at 740, 760 and 780 nm respectively were used as excitation light sources. In addition, short-pass filter which has transmission edge at 775 nm has been applied to minimize the optical noise in each external noise factor. By comparing contrast of each image before and after use of the short-pass filter, we confirmed that optical noise reduced 49%, 56% and 66% in external noise factors respectively.

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1. Introduction

Fluorescence imaging technique uses the emission of light by a substance that has absorbed light or other electromagnetic radiation. In most cases, the emitted light has a longer wavelength, and therefore lower energy, than the absorbed radiation. However, fluorescence imaging technique has many advantages such as high contrast, that is, signal to noise ratio (SNR), high sensitivity and simple optical instrumentation and so on [1]-[5].

Recently, near-infrared (NIR) fluorescence monitoring in the range of 700 - 900 nm is being utilized in the bio-medical field actively because NIR has high penetration characteristic in hemoglobin, water and lipid etc [6]-[9].

In addition, Indocyanine green (ICG) which emits NIR light (center wavelength: 830 nm) has been used in target protein application since ICG was granted to use in clinical research by Food and Drug Administration (FDA) [10]-[14].

In particular, ICG is applied to monitor lymph nodes and blood vessels pertaining to evaluation of cerebral blood flow, liver, and circulation function because of the low toxicity and the high absorption rate of ICG in range of 600 - 900 nm [15] [16]. Also, ICG is widely used as the synthesized probe and the surgical guide by NIR fluorescence agent and specific substance which is capable of tracking of tumors [17] [18].

Additionally, Beth Israel Deaconess Medical Center in USA and Hamamatsu in Japan developed FLARE™ (Fluorescence-assisted resection and exploration) system and PDE (Photodynamic Eye), respectively. They have used the devices to image identification of the sentinel lymph node (SLN) and the metastasis of malignant tumors like the breast cancer and the stomach cancer [19]-[22].

Although preclinical/clinical studies with the NIR fluorescence imaging system have briskly proceeded, studies to improve performance of the NIR fluorescence imaging such as elimination of optical noise, improvement of optical source etc have not briskly proceeded.

Especially, optical noise decreases NIR fluorescence image quality because optical noise reduces effectiveness of NIR fluorescence signals and disturbs detection of minute signals in preclinical/clinical studies. In order to minimize optical noise realized fluorescence image in a dark room. So, studies to minimize optical noise in NIR fluorescence imaging should be considered in preclinical/environment necessarily.

In this paper, we suggest conditions to minimize optical noise by the fluorescent light source, the interior light and the surgical light in the operation room.

2. Materials and Methods

2.1. Composition of a NIR Fluorescence Imaging System

A NIR fluorescence imaging system was configured to know how optical noise factors influence during realization of NIR fluorescence imaging as shown in Figure 1.

A band-pass filter (#84-107, Edmund Optics) with 832 nm ± 20 nm bandwidth and a charge-coupled device (CCD) camera (Guppy Pro F-031B, Allied Vision Technology) with a small lens (#58-000, Edmund Optics) were used in the fluorescence imaging system.

In addition, an optical light source composed of 16 light emitting diodes (LEDs) with each 1 W optical power for fluorescence excitation was used in the fluorescence imaging system. Three kinds of LEDs which have the center wavelength of 740, 760 and 780 nm were prepared for comparison of fluorescence signals according to the wavelengths of the LEDs.

2.2. Reagent

For the expression of the NIR fluorescence ICG (Diagnogreen, DAIICHISANKYO CO., Osaka, Japan) with the maximum absorption at 780 nm and the maximum emission at 830 nm was resuspended in 10 cc of sterile water to yield a 0.8 μl/ml stock solution.
A circular gauze coated with ICG solution (10 mm in diameter) which was put on a circular gauze without ICG solution (30 mm in diameter) was prepared as a sample for measurement of the NIR fluorescence.

2.3. Selection of Optical Noise Environment Factor

The fluorescence light source, the interior light and the surgical light were selected as optical noise factors in NIR fluorescence imaging.

Most of all, spectra or the fluorescent light source, the interior light and the surgical light that were selected as optical noise factors were measured to verify influence of the factors on optical noise. The NIR fluorescence images under three optical noise factors were acquired and the acquisitions repeated after applying a short-pass filter to minimize optical noise.

2.3.1. Evaluation of the Properties of Fluorescence Excitation Light and External Lighting

Spectra of three kinds of LEDs with center wavelength of 740, 760, 780 nm, the interior light and surgical light were measured by using a spectrometer (USB 4000, Ocean Optics).

Measurement results represent as shown in Figure 2.

2.3.2. Measurement and Analysis of Optical Noise Environment

First, NIR fluorescence imaging proceeded with three kinds of LEDs in the darkroom in order to verify optical noise effects of the LEDs, excitation light sources.

Second, NIR fluorescence imaging proceeded with three kinds of LEDs under the interior light in order to verify optical noise effects of the interior light.

Finally, NIR fluorescence imaging proceeded with three kinds of LEDs under the surgical light (C100, 1700 lux, Luvis, Korea) in order to verify optical noise effects of the surgical light.

In the NIR fluorescence imaging, we controlled output powers of 740, 760 and 780 nm LEDs as 270 μW, respectively. Then, we acquired NIR fluorescence imaging with the circular gauze sample.

For comparison among the NIR fluorescence images obtained under the each condition drawing, we calculated the average value in a region of interest (ROI) of the images. Figure 3 shows application of any circular ROI on the sample by using the ImageJ, an image processing program developed by the United States National Institutes of Health.

Then, we compared the contrast defined as Equation (1) by the expression of fluorescence signal (IFS, FS: fluorescence signal) intensity and background signal (IBS, BS: background signal) intensity in the NIR fluorescence image.

\[ C = \frac{I_{FS} - I_{BS}}{I_{FS} + I_{BS}} \]  

(1)

2.3.3. The Application of a Short-Pass Filter for Minimum Optical Noise and Method of Analysis

775 nm short-pass filter (#64-615, Edmund Optics) having the optical characteristics as shown in Figure 4 was
Figure 2. Emission spectrum curves of each light source. Curves of 740, 760, 780 nm excitation lights (a), curve of fluorescent light (b), curve of surgical light (c).

Figure 3. Method of drawing ROI (region of interest). Region of fluorescence signal (a) and background signal (b).
used to the minimized optical noise by the optical noise factors.

First, we measured spectrum of the fluorescent light source after applying the short-pass filter to the fluorescent light source having a center wavelength of 740, 760 and 780 nm in the darkroom. Also we obtained the fluorescence image of the gauze sample by using the three light sources with the short-pass filter.

Second, we applied the short-pass filter to the interior light and the fluorescent light sources having a center wavelength of 740, 760 and 780 nm.

Then, we measured spectrum of the interior light and obtained the fluorescence image of the gauze sample by using the three light sources with the short-pass filter under the interior light with the short-pass filter.

Third, we applied the short-pass filter to the surgical light and the fluorescent light sources having a center wavelength of 740, 760 and 780 nm.

Then, we measured spectrum of the surgical light and obtained the fluorescence image of the gauze sample by using the three light sources with the short-pass filter under the surgical light with the short-pass filter.

Finally, we obtained average signals about two regions shown in Figure 3 with the same analysis method of optical noise factor and compared the change of the contrast in Equation (1), by application of the short-pass filter.

3. Results

3.1. Measurement Results of Light Source Properties

Spectral measurement results of each excitation light source showed that LED light sources with center wavelength of 760 and 780 nm except for LED light source with center wavelength of 740 nm have spectral region more than 810 nm. Therefore, it was confirmed that there is overlap between spectrum of light sources with center wavelength of 760 and 780 nm and emission spectrum of ICG.

In addition, spectral measurement results of the interior light and the surgical light show that they have spectral region more than 810 nm although optical intensity at the spectral region is minute.

For analysis of optical noise in fluorescence imaging, output power of excitation light sources with center wavelength of 740, 760 and 780 nm was identically prepared as 270 μW and output power of the surgical light output power was prepared to control as 0.85, 1.08, 1.81, 2.41, 3.14 and 3.68 mW/cm².

3.2. Measurement and Analysis Results of Light Noise Environment

To measure and analyze optical noise factors in fluorescence imaging, we acquired NIR fluorescent images by using LED excitation light sources with center wavelength of 740, 760 and 780 nm in dark room and we repeated NIR fluorescent imaging under a interior light and a surgical light, respectively.

Figure 5 shows fluorescence images of the circular gauze coated with ICG solution measured by using LED excitation light sources with center wavelength of 740, 760 and 780 nm in the dark room, respectively.

In case of the excitation light source with center wavelength of 740 nm, the fluorescence image had an aver-
age intensity of 97.67 and contrast of 0.94 in the dark room.

In case of the excitation light sources with center wavelength of 760 and 780 nm, each average intensity increased to 209.17 and 255.0 and each contrast decreased to 0.45 and 0.00 beside case of the excitation light sources with center wavelength of 740 nm.

Figure 6 shows fluorescence images of the circular gauze coated with ICG solution measured by using LED excitation light sources with center wavelength of 740, 760 and 780 nm under the interior light, respectively.

In case of the excitation light source with center wavelength of 740 nm, the fluorescence image had an average intensity of 113.16 and contrast of 0.75 under the interior light.

In case of the excitation light sources with center wavelength of 760 and 780 nm, each average intensity was 228.79 and 255.0 and each contrast was 0.41 and 0.00, respectively.

Figure 7 shows fluorescence images of the circular gauze coated with ICG solution measured by using LED excitation light sources with center wavelength of 740, 760 and 780 nm under the surgical light, respectively.
The fluorescence images were saturated from 1.81 mW/cm² intensity in case of the excitation light source with center wavelength of 740 nm and were saturated from 0.85 mW/cm² intensity in case of the excitation light source with center wavelength of 760 and 780 nm under the surgical light.

3.3. Improvement of Optical Noise by Short-Pass Filter

**Improvement Results of Optical Noise by Using Short-Pass Filter**

We placed the short-pass filter in front of excitation light sources (740, 760 and 780 nm) and acquired fluorescence images of the circular gauze coated with ICG solution by using LED excitation light sources with center wavelength of 740, 760 and 780 nm in the dark room, respectively. **Figure 8** shows the acquired fluorescence images in the darkroom.

Average fluorescence intensity from each fluorescent image was 77.52 (in case of the 740 nm light source), 87.83 (in case of the 760 nm light source), 103.74 (in case of the 780 nm light source) and each contrast was 0.97 (in case of the 740 nm light source), 0.97 (in case of the 760 nm light source), 0.97 (in case of the 780 nm light source). We could confirm that each optical noise decreased 3% (in case of the 740 nm light source), 49% (in case of the 760 nm light source), 93% (in case of the 780 nm light source) by using the short-pass filter, respectively.

In addition, we placed the short-pass filter in front of excitation light sources (740, 760 and 780 nm) and the interior light and then we acquired fluorescence images of the circular gauze coated with ICG solution by using LED excitation light sources with center wavelength of 740, 760 and 780 nm under the interior light, respectively. **Figure 9** shows the acquired fluorescence images under the interior light. Average fluorescence intensity from each fluorescent image was 68.28 (in the case of the 740 nm light source), 84.79 (in the case of the 760 nm light source), 93.75 (in the case of the 780 nm light source) and each contrast was obtained 0.94 (in the case of the 740 nm light source), 0.94 (in the case of the 760 nm light source), 0.95 (in the case of the 780 nm light source). We could confirm that each optical noise decreased 20% (in the case of the 740 nm light source), 51% (in the case of the 760 nm light source), 93% (in the case of the 780 nm light source) by using the short pass filter, respectively.

Finally, we placed the short-pass filter in front of excitation light sources (740, 760 and 780 nm) and the interior light and then we acquired fluorescence images of the circular gauze coated with ICG solution by using LED excitation light sources with center wavelength of 740, 760 and 780 nm under the surgical light, respectively. **Figure 10** shows the acquired fluorescence images under the surgical light.

From **Figure 7(c)** (in the case of the 780 nm light source), we could confirm that it was impossible to distinguish the background from the fluorescence at 0.85 mW/cm² power of surgical light when the short-pass filter did not refer to the light source and the surgical light. From **Figure 10(c)**, on the other hand, we could confirm...
Figure 10. Short-pass filter is applied to 740 (a), 760 (b), 780 (c) nm excitation light and surgical light, and then NIR fluorescence imaging acquires (i: in case of 0.85 mW/cm²; ii: in case of 1.38 mW/cm²; iii: in case of 2.00 mW/cm²; iv: in case of 2.47 mW/cm²; v: in case of 3.28 mW/cm²; vi: in case of 3.66 mW/cm² of surgical light output power).

that each contrast was in value from 0.55 to 0.8 and that it is possible to distinguish the background from the fluorescence at 0.85 mW/cm² power of surgical light when the short-pass filter referred to the light source and the surgical light.

4. Conclusions

In this paper, we have suggested that LEDs as the excitation light, the interior light and surgical light can degrade light source and the external.

To analyze influence of the excitation light, the interior light and surgical light as optical noise factor, we acquired and compared fluorescence images by using the ICG and NIR fluorescence imaging system under various experimental conditions such as no light, interior light and surgical light.

An experiment was carried out by using LEDs with center wavelength of 740, 760 and 780 nm as the excitation light source.

From measured results of spectrum and intensity of the excitation light source, the interior light and the surgical light with review of the optical noise occurrence factor, we could confirmed that the optical noise is generated because of the overlapping between wavelength band of the optical noise factors and wavelength band of fluorescence signal. To solve the optical noise problem, we applied the short-pass filter to optical noise factors.

We used the short-pass filter which has cut-off edge at 775 nm wavelength to minimize influence by optical characteristics of the optical factors such as intensity decrease.

We could confirm that contrast of fluorescence images improved 49%, 56% and 66% by using the short-pass filter as compared with contrast of fluorescence imaging in case of no short-pass filter.

5. Discussion

In research results of other groups, the LED excitation light source with center wavelength of 760 nm or 770 nm was considered as an optimal light source in case of ICG based on NIR signal detection [23]. However, after application of short-pass filter in our research results, we could confirm that NIR fluorescence imaging with improved fluorescence signal and contrast is possible by using LED excitation light source with center wavelength of 780 nm. Also, we demonstrated that the excitation light source, interior light and surgical light affect seriously as optical noise factors in fluorescence imaging and that the application of the short-pass can make free from restraint of fluorescence imaging environment in performing the fluorescence imaging.
References


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