# Boundary Layer Flow and Heat Transfer of a Dusty Fluid over a Stretching Vertical Surface

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## Abstract

This paper presents the study of convective heat transfer characteristics of an incompressible dusty fluid past a vertical stretching sheet. The governing partial differential equations are reduced to nonlinear ordinary differential equations by using similarity transformation. The transformed equations are solved numerically by applying Runge Kutta Fehlberg fourth-fifth order method (RKF45 Method). Here obtained non-dimensional velocity and temperature profiles has been carried out to study the effect of different physical parameters such as fluid-particle interaction parameter, Grashof number, Prandtl number, Eckert number. Comparison of the obtained numerical results is made with previously published results.

Keywords: Boundary Layer Flow, Dusty Fluid, Stretching Sheet, Grashof Number, Fluid-Particle Interaction Parameter, Numerical Solution

# 1. Introduction

The behavior of boundary layer flow due to a moving flat surface immersed in a quiescent fluid was first studied by Sakiadis [1], who investigated it theoretically by both exact and approximate methods. Crane [2] presented a closed form exponential solution for the planar viscous flow of linear stretching case. Later this problem has been extended to various aspects by considering non-Newtonian fluids, more general stretching velocity, magnetohydrodynamic (MHD) effect, porous sheet, porous media and heat or mass transfer. Andreson et al. [3] extended the work of crane [2] to non-Newtonian power law fluid over a linear stretching sheet. Chakrabarti and Gupta [4] have discussed the hydromagnetic flow and heat transfer over a stretching sheet. Grubka and Bobba [5] analyzed heat transfer studies by considering the power law variation of surface temperature. Cortell [6] studied the magnetohydrodynamics flow of a power-law fluid over a stretching sheet. Chen [7] analyzed mixed convection of a power law fluid past a stretching surface in the presence of thermal radiation and magnetic field.

Power law model has some limitations as, it does not exhibit any elastic properties such as normal stress differences in shear flow. In certain polymer processing applications, flow of a viscoelastic fluid over a stretching sheet is important. For that reason Cortell [8] studied the effects of viscous dissipation and work done by deformation on the MHD flow and heat transfer of a viscoelastic fluid over a stretching sheet. Abel *et al.* ([9,10]) extended the work and studied the viscoelastic MHD flow and heat transfer over a stretching sheet with viscous and ohmic dissipation, non-uniform heat source and radiation. Tsai *et al.* [11] studied an unsteady flow over a stretching surface with non-uniform heat source. Ishak *et al.* [12] obtained the solution to unsteady laminar boundary layer over a continuously stretching permeable surface.

These investigations deal with the flow and heat transfer induced by a horizontal stretching sheet, but there arise some situations where the stretching sheet moves vertically in the cooling liquid. Under such circumstances the fluid flow and the heat transfer characteristics are determined by two mechanisms, namely the motion of stretching sheet and the buoyant force. The thermal buoyancy resulting from heating/cooling of a vertically moving stretching sheet has a large impact on the flow and heat transfer characteristics. Effects of thermal buoyancy on the flow and heat transfer under various physical situations have been reported by many investigators (see [13-16]).

To study the two-phase flows, in which solid spherical



particles are distributed in a fluid are of interest in a wide range of technical problems, such as flow through packed beds, sedimentation, environmental pollution, centrifugal separation of particles, and blood rheology. The study of the boundary layer of fluid-particle suspension flow is important in determining the particle accumulation and impingement of the particle on the surface. In view of these applications, Chakrabarti [17] analyzed the boundary layer in a dusty gas. Datta and Mishra [18] have investigated boundary layer flow of a dusty fluid over a semi-infinite flat plate. Further, researches in these fields have been studied by many investigators such as Evgeny and Sergei [19], XIE Ming-liang et al. [20], Palani et al. [21], Agranat [22] and Vajravelu et al. [23]. Abdul Aziz [24] obtained the numerical solution for laminar thermal boundary over a flat plate with a convective surface boundary condition using the symbolic algebra software Maple.

Motivated by the above investigations, we present in this paper the boundary layer flow and heat transfer of a dusty fluid over a stretching vertical surface. The governing partial differential equations are transformed into ordinary differential equations using similarity transformation, before they are solved numerically by Runge Kutta Fehlberg fourth-fifth order method. Comparison of the results are to be in excellent agreement those reported by Grubka and Abel. The RKF45 algorithm in Maple has been well tested for its accuracy and robustness. The analysis of obtained results showed that the fluid particle interaction parameter, Grashof number, Prandtl number and Eckert number have significant influence on the flow and heat transfer.

#### 2. Flow Analysis of the Problem

Consider a steady two dimensional laminar boundary layer flow of an incompressible viscous dusty fluid over a vertical stretching sheet. The flow is generated by the action of two equal and opposite forces along the *x*-axis and *y*-axis being normal to the flow. The sheet being stretched with the velocity  $U_w(x)$  along the *x*-axis, keeping the origin fixed in the fluid of ambient temperature *T*. Both the fluid and the dust particle clouds are suppose to be static at the beginning. The dust particles are assumed to be spherical in shape and uniform in size and number density of the dust particle is taken as a constant throughout the flow.

The momentum equations of the two dimensional boundary layer flow in usual notation are [23]:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$
 (2.1)

$$u\frac{\partial u}{\partial x} + v\frac{\partial v}{\partial y} = v\frac{\partial^2 u}{\partial y^2} + \frac{KN}{\rho}\left(u_p - u\right) + g\beta^*\left(T - T_{\infty}\right) \quad (2.2)$$

$$u_{p}\frac{\partial u_{p}}{\partial x} + v_{p}\frac{\partial u_{p}}{\partial y} = \frac{K}{m}\left(u - u_{p}\right)$$
(2.3)

$$u_{p}\frac{\partial v_{p}}{\partial x} + v_{p}\frac{\partial v_{p}}{\partial y} = \frac{K}{m}\left(v - v_{p}\right)$$
(2.4)

$$\frac{\partial}{\partial x} \left( N u_p \right) + \frac{\partial}{\partial y} \left( N v_p \right) = 0 \tag{2.5}$$

where (u, v) and  $(u_p, v_p)$  are the velocity components of the fluid and dust particle phases along x and y directions respectively. u,  $\rho$  and N are the co-efficient of viscosity of the fluid, density of the fluid, number density of the particle phase, K is the stokes' resistance (drag co-efficient), T and  $T_{\infty}$  are the fluid temperature within the boundary layer and in the free stream respectively. g is the acceleration due to gravity,  $\beta^*$  is the volumetric coefficient of thermal expansion, m is the mass of the dust particle respectively. In deriving these equations, the drag force is considered for the iteration between the fluid and particle phases.

The boundary conditions are

$$u = U_w(x), v = 0 \text{ at } y = 0,$$
  

$$u \to 0, u_p \to 0, v_p \to v, N \to \omega\rho \text{ as } y \to \infty.$$
(2.6)

where  $U_w(x) = cx$  is a stretching sheet velocity, c > 0 is stretching rate,  $\omega$  is the density ratio. To convert the governing equations into a set of similarity equations, we introduce the following transformation as mentioned below,

$$u = cxf'(\eta), v = -\sqrt{vc}f(\eta), \eta = \sqrt{\frac{c}{v}}y$$

$$u_p = cxF(\eta), v_p = \sqrt{vc}G(\eta), \rho_r = H(\eta)$$
(2.7)

which identically satisfies (2.1), and substituting (2.7) into (2.2) to (2.5), we obtain the following non-linear ordinary differential equations:

$$f'''(\eta) + f(\eta)f''(\eta) - [f'(\eta)]^{2} + Gr\theta(\eta)$$
  
+ $l^{*}\beta H(\eta)[F(\eta) - f'(\eta)] = 0$ 
(2.8)

$$G(\eta)F'(\eta) + \left[F(\eta)\right]^2 + \beta\left[F(\eta) - f'(\eta)\right] = 0 \quad (2.9)$$

$$G(\eta)G'(\eta) + \beta \left[ f(\eta) + G(\eta) \right] = 0 \qquad (2.10)$$

$$H(\eta)F(\eta)+H(\eta)G'(\eta)+G(\eta)H'(\eta)=0 \quad (2.11)$$

where a prime denotes differentiation with respect to  $\eta$ and  $l^* = mN/\rho$ ,  $\tau = m/k$  is the relaxation time of the particle phase,  $\beta = 1/c\tau$  is the fluid particle interaction parameter,  $Gr = g\beta^* (T_w - T_w)/c^2 x$  is the Grashof number and  $\rho_r = N/\rho$  is the relative density.

The boundary conditions defined as in (2.6) will take

the form,

$$f(\eta) = 0, f'(\eta) = 0 \text{ at } \eta = 0$$

$$f'(\eta) = 0, F(\eta) = 0, G(\eta) = -f(\eta),$$

$$H(\eta) = \omega \text{ as } \eta \to \infty$$

$$(2.12)$$

If  $\beta = 0$  and Gr = 0 the analytical solution of (2.8) with boundary condition (2.12) can be written in the form:

$$f(\eta) = 1 - e^{-\eta}$$

#### 3. Heat Transfer Analysis

The dusty boundary layer heat transport equations in the presence of non-uniform internal heat generation/ab-sorption for two dimensional flows are given by [25]:

$$u\frac{\partial T}{\partial x} + v\frac{\partial T}{\partial y} = \frac{k^*}{\rho c_p}\frac{\partial^2 T}{\partial y^2} + \frac{N}{\rho \tau_T}(T_p - T) + \frac{N}{\rho c_p \tau_v}(u_p - u)^2$$
(3.1)

$$u_{p}\frac{\partial T_{p}}{\partial x}+v_{p}\frac{\partial T_{p}}{\partial y}=-\frac{c_{p}}{c_{m}\tau_{T}}\left(T_{p}-T\right)$$
(3.2)

where T and  $T_p$  is the temperature of the fluid and temperature of the dust particle,  $c_p$  and  $c_m$  are the specific heat of fluid and dust particles,  $\tau_T$  is the thermal equilibrium time and is time required by the dust cloud to adjust its temperature to the fluid,  $\tau_v$  is the relaxation time of the of dust particle *i.e.*, the time required by the a dust particle to adjust its velocity relative to the fluid,  $k^*$  is the thermal conductivity.

In order to solve the (3.1) and (3.2), we consider non dimensional temperature boundary condition as follows

$$T = T_{w} = T_{\infty} + A \left(\frac{x}{l}\right)^{2} \text{ at } y = 0$$
  

$$T \to T_{\infty}, \ T_{p} \to T_{\infty} \text{ as } y \to \infty$$
(3.3)

where A is a positive constant,  $l = \sqrt{\frac{v}{c}}$  is a characteristic large the

tic length.

Now we define the non-dimensional fluid phase temperature  $\theta(\eta)$  and  $\theta_p(\eta)$  dust phase temperature as

$$\theta(\eta) = \frac{T - T_{\infty}}{T_{w} - T_{\infty}}, \ \theta_{p}(\eta) = \frac{\left(T_{p} - T_{\infty}\right)}{T_{w} - T_{\infty}}$$
(3.4)

where  $T - T_{\infty} = A\left(\frac{x}{l}\right)^2 \theta(\eta)$ 

Using (3.4) into (3.1) to (3.2), we obtain the following non-linear ordinary differential equations

$$\theta''(\eta) + \Pr\left[f(\eta)\theta'(\eta) - 2f'(\eta)\theta(\eta)\right] + \frac{NPr}{\rho c \tau_{T}} \left[\theta_{p}(\eta) - \theta(\eta)\right] + \frac{NPrEc}{\rho \tau_{v}} \left[F(\eta) - f'(\eta)\right]^{2} \qquad (3.5)$$

$$2F(\eta)\theta_{p}(\eta) + G(\eta)\theta'_{p}(\eta) + \frac{c_{p}}{c c_{m} \tau_{T}} \left[\theta_{p}(\eta) - \theta(\eta)\right] = 0 \qquad (3.6)$$

where  $Pr = \frac{\mu c_p}{k^*}$  is the Prandtl number,  $Ec = \frac{cl^2}{Ac_p}$  is

the Eckert number.

The corresponding boundary conditions for  $\theta(\eta)$  and  $\theta_n(\eta)$  as

$$\begin{aligned} \theta(\eta) &= 1 \text{ as } \eta = 0 \\ \theta(\eta) &\to 0, \ \theta_p(\eta) \to 0 \text{ as } \eta \to \infty \end{aligned}$$
 (3.7)

#### 4. Results and Discussion

The system of coupled ordinary differential Equations (2.8) to (2.12) and (3.5) to (3.7) has been solved numerically using Runge-Kutta-Fehlberg fourth-fifth order method. To solve these equations we adopted symbolic algebra software Maple which was given by Aziz [24]. Maple uses the well known Runge-Kutta-Fehlberg fourty-fifth order (RFK45) method to generate the numerical solution of a boundary value problem. The boundary conditions  $\eta = \infty$  were replaced by those at  $\eta = 5$  in accordance with standard practice in the boundary layer analysis. Numerical computation of these solutions have been carried out to study the effect of various physical parameters such as fluid particle interaction parameter  $\beta$ , Grashof number Gr, Prandtl number Pr and Eckert number Ec are shown graphically.

In order to verify the accuracy of our present study, the values for wall temperature  $\theta'(0)$  gradient for various values of Prandtl number are given in **Table 1**, which shows the excellent agreement with those reported by Grubka and Bobba [5] and Abel and Mahesha [10]. Further, the **Table 2** shows the results of thermal characteristics at the wall for different values of influenced physical parameters.

**Figure 1** shows the effect of Grashof number (Gr) on the velocity profile. From this plot it is observed that the effect of increasing values of Grashof number is to increases the velocity distribution in the flow region. Physically Gr > 0 means heating of the fluid or cooling of the boundary surface, Gr < 0 means cooling of the fluid or heating of the boundary surface and Gr = 0 corresponds to the absence of free convection current.

From the Figure 2 shows the effect of fluid particle



Figure 1. Effect of *Gr* on the velocity profiles for  $\beta = N = 0.5$ , Ec = 2.0, Pr = 1.0 and  $\omega = 0.2$ .



Figure 2. Effect of  $\beta$  on the velocity profiles for Gr = N = 0.5, Ec = 2.0, Pr = 1.0 and  $\omega = 0.2$ .

interaction parameter  $(\beta)$  on velocity components of the fluid velocity  $f'(\eta)$  and particle velocity  $F(\eta)$ *i.e.*, if  $\beta$  increases we can find the decrease in the fluid phase velocity and increase in the dust phase velocity. Also it reveals that for the large values of  $\beta$  *i.e.*, the relaxation time of the dust particle decreases then the velocities of both fluid and dust particles will be the same.

**Figure 3** which illustrate the effect of Prandtl number (Pr) on the temperature profiles. We infer from this figure that the temperature decreases with an increase in the Prandtl number, which implies viscous boundary layer is thicker than the thermal boundary layer. From these plots it is evident that large values of Prandtl number result in thinning of the thermal boundary layer. In this case temperature asymptotically approaches to zero

in free stream region. This is in contrast to the effects of other parameters, except Gr and  $\beta$  on heat transfer.

**Figures 4** is plotted for the temperature profiles for different values of (Ec). We observe that the effect of increasing values of Eckert number is to enhance the temperature at a point which is true for both the fluid phase as well as dust phase temperatures. Physically it means that the heat energy is stored in the fluid due to the frictional heating.

**Figure 5** depict the effect of Grashof number (Gr) versus  $\eta$ . It is evident from these plots that increasing value of Gr results in thinning of the thermal boundary layer associated with an increase in the wall temperature gradient and hence produces an increase in the heat transfer rate.

**Figure 6**, which is a graphical representation of the temperature profiles for different values of  $\beta$  versus



Figure 3. Effect of *Pr* on the temperature profiles for  $\beta = N = 0.5$ , Ec = 2.0, Gr = 0.5 and  $\omega = 0.2$ .



Figure 4. Effect of *Ec* on the temperature profiles for  $\beta = N = 0.5$ , Gr = 0.5, Pr = 1.0 and  $\omega = 0.2$ .

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Figure 5. Effect of *Gr* on the temperature profiles for  $\beta = N = 0.5$ , Ec = 2.0, Pr = 1.0 and  $\omega = 0.2$ .



Figure 6. Effect of  $\beta$  on the temperature profiles for Gr = N = 0.5, Ec = 2.0, Pr = 1.0 and  $\omega = 0.2$ .

Table 1. Comparison of the results for the dimensionless temperature gradient  $\theta'(\eta)$  in the case of  $\beta = 0$ , N = 0 and Gr = 0.

Pr	Grubka and Bobba [5]	Abel and Mahesha [10]	Present Study $\theta'(0)$
0.72	1.0885	1.0885	1.0886
1.0	1.3333	1.3333	1.3333
10.0	4.7969	4.7968	4.7968

 $\eta$ . We infer from these figures that temperature of the fluid and dust particle decreases with increase in  $\beta$  respectively. From all the graphs we can observed that fluid phase temperature is higher than the dust phase temperature and also it indicates that the fluid particles tempera-

		-		
β	Ec	Pr	Gr	heta'(0)
0.2	2.0	1.0	0.5	-0.07441
0.5				-1.11703
1.0				-1.39241
0.5	0.0	1.0	0.5	-1.70879
	1.0			-1.41767
	2.0			-1.11703
0.5	2.0	1.0	0.5	-1.11703
		2.0		-1.56421
		3.0		1.89316
0.5	2.0	1.0	0.0	-1.12770
			0.5	-1.11703
			1.0	-1.09157

Table 2. Values of wall temperature gradient  $\theta'(0)$  for different values of the parameters  $\beta$ , Gr, Pr and Ec.

ture is parallel to the dust particles temperature. We have used throughout our thermal analysis the values of  $\tau_T = \tau_v = 0.5$  and  $c_p = c_m = 0.2$ ,  $\rho = 0.5$ , c = 1.

### 5. Conclusions

The two-dimensional boundary layer flow and heat transfer of a dusty fluid due to a vertical stretching sheet has been investigated. The governing partial differential equation is converted into ordinary differential equations by using similarity transformations. The effect of several parameters controlling the velocity and temperature profiles are shown graphically and discussed briefly. The influence of the parameter  $\beta$ , Gr, Ec and Pr on dimensionless velocity and temperature profiles were examined.

Some of the important findings of our analysis obtained by the graphical representation are listed below.

- The effect of *Gr* is to increase the momentum boundary layer thickness and to decrease the thermal boundary layer thickness.
- *Ec* has significant effect on the boundary layer growth.
- The boundary layers are highly influenced by the Prandtl number. The effect of *Pr* is to decreases the thermal boundary layer thickness.
- The rate of heat transfer  $\theta'(0)$  decreases with increasing the *Pr* and  $\beta$ . While it increases with increasing the *Ec*.

If Gr = 0 we can find the results of the horizontal stretching sheet.

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# Nomenclature

Nomenclature		$u_p, v_p$	velocity components of the dust particle along	
		I I	x and y directions	
Α	constant	x	coordinate along the stretching sheet	
с	stretching rate	У	distance normal to the stretching sheet	
$C_m$	specific heat of dust phase	Greek sy	ymbols	
$C_{n}^{m}$	specific heat of fluid	μ	coefficient of the viscosity of the fluid	
$\stackrel{\scriptscriptstyle P}{Ec}$	Eckert number	ρ	density of the fluid	
Gr	Grashof number	ω	density ratio	
Κ	stokes resistance	τ	relaxation time of the dust phase	
$k^{*}$	thermal conductivity	$\beta$	fluid particle interaction parameter	
l	characteristic length	$\rho_r$	relative density	
Ν	number density of the dust phase	$ au_T$	thermal equilibrium time	
Pr	Prandtl number	$ au_v$	relaxation time of the dust phase	
Т	temperature of the fluid	$\theta$	fluid phase temperature	
$T_{-}$	temperature of the dust phase	$\theta_{p}$	dust phase temperature	
$T_{}^{\nu}$	temperature at the wall	$\eta^{'}$	dimensionless space variable	
$T_{\infty}^{w}$	temperature at large distance from the wall	Subscriț	pts	
$\widetilde{U_{u}}(x)$	stretching sheet velocity	W	properties at the plate	
<i>u</i> , <i>v</i>	velocity components of the fluid along $x$ and $y$ directions	80	free stream condition	