

The Effects of Post-Stenotic Dilatations on the Flow of Couple Stress Fluid through Stenosed Arteries

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Abstract

The flow of incompressible couple stress fluid in a circular tube with stenosis and dilatations has been investigated. The stenosis was assumed to be axially symmetric and mild. The flow equations have been linearized and the expressions for the resistance to the flow, velocity, pressure drop, wall shear stress have been derived. The effects of various parameters on these flow variables have been investigated. It is found that the resistance to the flow and pressure drop increase with height of the stenosis and decrease with post stenotic dilatation. Pressure drop decreases with couple stress fluid parameter for both stenosis and post stenotic dilatation. Further, the wall shear stress increases with height of the stenosis and couple stress parameter but decreases with post stenotic dilatation and couple stress fluid parameter.

Keywords

Stenosis, Dilatation, Wall Shear Stress, Resistance to the Flow, Couple Stress Fluid Parameter

1. Introduction

In the present world, diseases in the blood vessels and in the heart like heart attack and stroke are major health hazards causing a large number of deaths. The main reason for these deaths is stenosis. The actual causes for stenosis are not well known but it has been suggested that deposits of fatty substances, cholesterol, cellular waste products on the arterial wall are called as stenosis. When stenosis is formed in the artery then these fatty substances can block an artery and blood flow will be restricted. This may lead to heart attacks, hypertension and brain strokes etc. Hence formation of the stenosis *i.e.* abnormal and unnatural growth on the arterial wall can disturb the normal functioning

of the cardiovascular system and there is considerable evidence that hydro-dynamical factors such as change in pressure, wall shear stress and impedance can play a significant role in the development and progression of this pathological condition. Hence detailed knowledge of the blood flow in stenosed arteries is required to understand and prevent arterial diseases.

Based on this large number of studies, it has been available to understand flow of blood through arteries. The following literatures have been carried out on the assumption that blood behaves like a non-Newtonian fluid. And it is well known that, blood being the suspension of cells, behaves like a non-Newtonian fluid at low shear rates and during its flow through narrow blood vessels. Shukla *et al.* [1] studied the effects of stenosis on Non-Newtonian flow of the blood in an artery. Chakravarty Santabrata *et al.* [2] discussed dynamic response of arterial blood flow in the presence of multi-stenoses. Philip *et al.* [3] studied the flow of blood, and modeled it by a simple micro fluid in the core region with Newtonian fluid peripheral layer, in a tube in the presence of mild stenosis. Prashanth Kumar [4] studied on unsteady analysis of non-Newtonian blood flow through tapered arteries with a stenosis. Sankar and Hemalatha [5] investigated on steady flow of Herschel-Bulkley fluid through catheterized arteries. Maruthi Prasad *et al.* [6] have developed the flow of Herschel-Bulkley fluid through an inclined tube of non-uniform cross section with multiple stenoses. Effect of paired stenosis on blood flow through small artery was presented by Yaseen Ali Khan Mea [7]. Sreenadh *et al.* [8] developed a model and analyzed flow of a Casson fluid through an inclined tube of non-uniform cross section with multiple stenoses. Rekha Bali *et al.* [9] developed mathematical model with multiple stenosis in presence of magnetic field by treating blood as Casson fluid. Mathematical analysis of Casson fluid model for blood rheology in stenosed narrow arteries was studied by Venkatesan *et al.* [10].

Couple stress fluid is a special case of non-Newtonian fluid which was developed by Stokes [11]. The important feature of these fluids is that stress tensor is not symmetric and their accurate flow behavior cannot be predicted by classical Newtonian theory. The main effect of couple stress will introduce a size-dependent effect that is not present in the classical viscous theories. Couple stress fluid model has been widely used by researchers because of its relative mathematical simplicity compared with other models. Blood, lubricants containing small amount of high polymer additives, electro-rheological fluids and synthetic fluids show the effect of couple stress and rotation of molecules, which are not present in the case of Newtonian fluids. Bringing a few on couple stress fluid, Srivastava [12] considered the flow of couple stress fluid through stenotic vessels with peripheral layer. Srinivasacharya *et al.* [13] investigated on effects of couple stresses on the flow in a constricted annulus. Effect of peripheral layer on peristaltic transport of couple stress fluid was studied by Maruthiprasad *et al.* [14]. Pulsatile flow of couple stress fluid through a porous medium with periodic body acceleration and magnetic field was presented by Rathod *et al.* [15]. Srikanth *et al.* [16] have analyzed the mathematical problems of non-Newtonian fluid through multiple stenosis arteries in the presence of couple stress. Peristaltic transport of a couple stress fluid has

been discussed by Maiti *et al.* [17]. Gruju Awgichew *et al.* [18] described the effect of slip condition on couple stress fluid flow through porous medium with stenosis.

Arterial dilatation distal to a stenosis has been known as post stenotic dilatation. It is observed that, the nervous system in some people is weak (especially in old people). When blood is clotted at particular position, after that position the arterial wall bulges out (due to high pressure). If it goes on increasing, there is chance to harm the arterial walls. It may causes for death. The exact flow disturbances is uncertain, statis, increased lateral pressure, cavitations, abnormal shear stresses and turbulence all have been postulated to be the causes of post stenotic dilatation. Therefore, understanding the dilatation problems will more helpful to diagnoses the arterial diseases. Based on this, Pincombe *et al.* [19] studied the analysis of post-stenotic dilatations on the blood flow through the stonosed coronary arteries. Singh AK *et al.* [20] presented the effects of post stenotic dilatation by treating the fluid as Bingham fluid. Sanjeev Kumar *et al.* [21] described blood flow resistance for a small artery with multiple stenosis and post stenotic dilatation. Maruthi Prasad *et al.* [22] investigated on post stenotic dilatation by considering blood as Jeffrey fluid.

Motivated from the above studies a mathematical model was developed by considering blood as couple stress fluid, passing through an artery (tube) having stenosis and post stenotic dilatations. The velocity, impedance (resistance to the flow) and wall shear stress are calculated. The variation of impedance and shear stress is analyzed for various values of couple stress fluid parameters and geometric parameters.

2. Mathematical Formulation

Consider the flow of incompressible couple stress fluid through an axisymmetric artery (tube) containing stenosis and dilatation as shown in **Figure 1**.

The equations describing the geometry of the wall is given as follows

$$\begin{cases} 1 - \frac{\delta_i}{2R_0} \left[1 + \cos \frac{2\pi}{L_i} \left(Z - \alpha_i - \frac{L_i}{2} \right) \right] & \text{for } \alpha_i \leq Z \leq \beta_i \\ 1, & \text{otherwise} \end{cases} \quad (1)$$

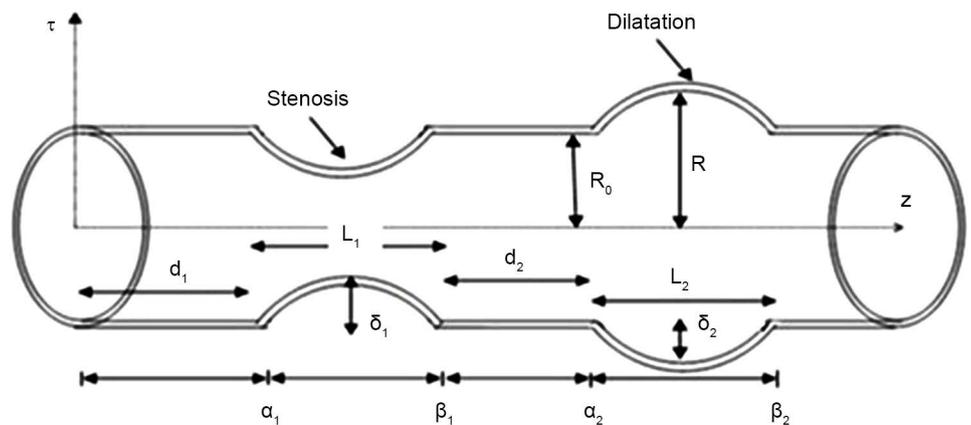


Figure 1. Geometry of arterial segment under consideration.

where δ_i represents the maximum distance of the i^{th} abnormal segment projects into lumen and is negative for aneurysms and positive for stenosis. R represents the radius of the artery, R_0 represents the radius of the normal artery, L_i represents the length of the i^{th} abnormal segment, α_i represents the distance from origin to the start of the i^{th} abnormal segment and is given by

$$\alpha_i = \sum_{j=1}^i (d_j + L_j) - L_i \tag{2}$$

And β_i represents the distance from the origin to the end of the i^{th} abnormal segment and is given by

$$\beta_i = \sum_{j=1}^i (d_j + L_j) \tag{3}$$

where d_i is the distance separating the start of i^{th} abnormal segment from the end of the $(i-1)^{\text{th}}$ or from the start of the segment if $i = 1$.

The constitutive equations of couple stress fluid are

$$\text{div} \bar{q} = 0 \tag{4}$$

$$T_{ji,j} = \rho \frac{du_i}{dt}, \quad e_{ijk} T_{jk}^A + M_{ji,j} = 0 \tag{5}$$

$$l_{ij} = -p\delta_{ij} + 2\mu_{ij}d_{ij}, \quad \mu_{ij} = 4\eta\mu_{j,i} + 4\eta'u_{ij}$$

where u_i is the velocity vector; T_{ij} and T_{ij}^A are the symmetric and antisymmetric parts of stress tensor T_{ij} respectively; M_{ij} is the couple stress tensor; μ_{ij} is the deviatoric part of M_{ij} and u_i is the vorticity vector; d_{ij} is the symmetric part of the velocity gradient; η and η' are constants associated with the couple stress; p is the pressure and other terms have their usual meaning from tensor analysis.

With the assumptions of stenosis is to be mild (which implies that the variation of all the flow characteristics except pressure along the axial directions is negligible), the length of the tube is large compared to its radius that is $\frac{\delta}{R_0} \ll 1$, and introducing the following non-dimensional quantities.

$$\begin{aligned} \bar{r} &= \frac{r}{a}, \quad \bar{z} = \frac{z}{L}, \quad \bar{\delta} = \frac{\delta}{R_0}, \quad \bar{p} = \frac{a^2 p}{L\mu U} \\ \bar{\alpha} &= a\alpha = a\sqrt{\frac{\mu}{\eta}}, \quad \bar{U} = \frac{u}{U} \\ \bar{d} &= \frac{d}{L}, \quad \bar{L} = \frac{L}{L_0} \end{aligned} \tag{6}$$

where U represents the average velocity.

The Equation (4) and Equation (5) becomes

$$\frac{\partial u}{\partial r} + \frac{u}{r} + \frac{\partial u}{\partial z} = 0 \tag{7}$$

$$\frac{\partial p}{\partial r} = 0 \tag{8}$$

$$\frac{1}{r} \frac{\partial}{\partial r} \left\{ r \frac{\partial}{\partial r} \left(1 - \frac{1}{\bar{\alpha}^2} \nabla^2 \right) u \right\} = \frac{\partial p}{\partial z} \quad (9)$$

where $\nabla^2 = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial}{\partial r} \right)$, u is the velocity $\bar{\alpha}^2 = \frac{\mu}{\eta} a^2$ (couple stress parameter), since $\sqrt{\frac{\mu}{\eta}}$, a characteristic measure of polarity of the fluid model, has a dimension of length, $\bar{\alpha}$ indicates the ratio of the tube to material characteristic length $\sqrt{\frac{\eta}{\mu}}$, in the limit as $\eta \rightarrow 0$ i.e. $\bar{\alpha} \rightarrow \infty$, the Equation (9) reduces to Navier-Stokes equation.

The non-dimensional boundary conditions are

$$\frac{\partial u}{\partial r} = 0 \quad \text{at } r = 0 \quad (10)$$

$$\frac{\partial^2 u}{\partial r^2} - \frac{\eta}{r} \frac{\partial u}{\partial r} = 0 \quad \text{at } r = h(z) \quad (11)$$

$$\frac{\partial^2 u}{\partial r^2} - \frac{\eta}{r} \frac{\partial u}{\partial r} = \text{is finite at } r = 0 \quad (12)$$

$$\text{That implies } u \text{ is finite at } r = 0 \quad (13)$$

$$u = 0 \quad \text{at } r = h(z) \quad (14)$$

2. Solution

Solving Equation (9) by using boundary conditions (10) to (14), we obtain the velocity as

$$u = AI_0(\bar{\alpha}r) + \left(\frac{r^2}{4} + \frac{1}{\bar{\alpha}^2} \right) \frac{dp}{dz} - d\bar{\alpha}^2 \quad (15)$$

where

$$A = \frac{h \left(\frac{\eta-1}{2} \right) \frac{dp}{dz}}{h\bar{\alpha}^2 I_0(\bar{\alpha}h) - \bar{\alpha} I_1(\bar{\alpha}h) - \eta \bar{\alpha} I_1(\bar{\alpha}h)}$$

$$d = \frac{1}{\bar{\alpha}^2} \left[AI_0(\bar{\alpha}h) + \left(\frac{h^2}{4} + \frac{1}{\bar{\alpha}^2} \right) \frac{dp}{dz} \right]$$

where I_0 and I_1 are Modified Bessel functions of order zero and one respectively.

$$\text{The dimensionless flux } q = \frac{q'}{\pi a^2 c} \text{ is given by} \quad (16)$$

Substituting Equation (15) in Equation (16) and then integrate we get

$$q = \int_0^h 2r \left\{ AI_0(\bar{\alpha}r) + \left(\frac{r^2}{4} + \frac{1}{\bar{\alpha}^2} \right) \frac{dp}{dz} - d\bar{\alpha}^2 \right\} dr \quad (17)$$

$$q = \frac{2Ah}{\bar{\alpha}} I_1(\bar{\alpha}h) - h^2 AI_0(\bar{\alpha}h) - \frac{h^4}{8} \frac{dp}{dz}$$

From Equation (17) we get $\frac{dp}{dz}$ as

$$\frac{dp}{dz} = \frac{8q}{h^4 T} \tag{18}$$

where

$$T = \frac{4(\eta-1)}{kh^3} \left[\frac{2h}{\bar{\alpha}} I_1(\bar{\alpha}h) - h^2 I_0(\bar{\alpha}h) \right] - 1$$

$$K = h\bar{\alpha}^2 I_0(\bar{\alpha}h) - \bar{\alpha} I_1(\bar{\alpha}h) - \eta \bar{\alpha} I_1(\bar{\alpha}h)$$

The pressure drop per wave length is given as $\Delta p = p(0) - p(\lambda)$ is

$$\Delta p = - \int_0^\lambda \frac{dp}{dz} dz = - \int_0^\lambda \frac{8q}{h^4 T} dz \tag{19}$$

The resistance to the flow λ is defined as

$$\lambda = \frac{\Delta p}{q} = - \frac{1}{q} \int_0^\lambda \frac{8q}{h^4 T} dz \tag{20}$$

The pressure drop in the absence of stenosis = 1 is denoted by Δp_n and is obtained from Equation (19) as

$$\Delta p_n = - \int_0^\lambda \frac{8q}{T} dz \tag{21}$$

The resistance to the flow in the normal artery is denoted by λ_n which is obtained from Equation (21) as

$$\lambda_n = \frac{\Delta p_n}{q} = - \frac{1}{q} \int_0^\lambda \frac{8q}{T} dz \tag{22}$$

The normalized resistance to the flow denoted by

$$\bar{\lambda} = \frac{\lambda}{\lambda_n} \tag{23}$$

The shear stress acting on the wall of tube is given by

$$\tau_w = \left(-\mu \frac{\partial u}{\partial r} \right) \text{ at } r = h(z) \tag{24}$$

Introducing the dimensionless quantity

$$\tau_w^* = \left(\frac{\tau_w}{\frac{\mu U}{d_0}} \right) \text{ at } r = h(z) \tag{25}$$

And using Equation (15) in Equation (24) we get (after dropping asterisks)

$$\tau_w = -\mu \left[A\bar{\alpha} I_1(\bar{\alpha}h) + \left(\frac{h}{2} \right) \frac{8q}{h^4 T} \right] \tag{26}$$

The shear stress at the wall in the absence of stenosis = 1 denoted by $(\tau_w)_n$ is obtained

from Equation (26) as

$$(\tau_w)_n = -\mu \left[A\bar{\alpha}I_1(\bar{\alpha}) + \left(\frac{1}{2}\right)\frac{8q}{T} \right] \tag{27}$$

The normalized shear stress at wall $\bar{\tau}_w$ is given by

$$\bar{\tau}_w = \frac{\tau_w}{(\tau_w)_n} \tag{28}$$

3. Results and Analysis

The expressions for Pressure drop (Δp), resistance to the flow ($\bar{\lambda}$), and wall Shear stress ($\bar{\tau}_w$) are given by Equation (19), Equation (23) and Equation (28) respectively and have been numerically evaluated by using MATHEMATICA Software for different values of corresponding parameters and presented graphically in the following **Figures 2-14**.

Figure 2 to Figure 4 shows the effects of various parameters on resistance to the flow in a uniform tube with mild stenosis. It is observed that, the resistance to the flow increases with height and length of the stenosis but decreases with height and length of post stenotic dilatation.

It can be seen from the **Figure 5 to Figure 8** that, the pressure drop increases with height of the stenosis and volumetric flow rate (q) but decreases with couple stress

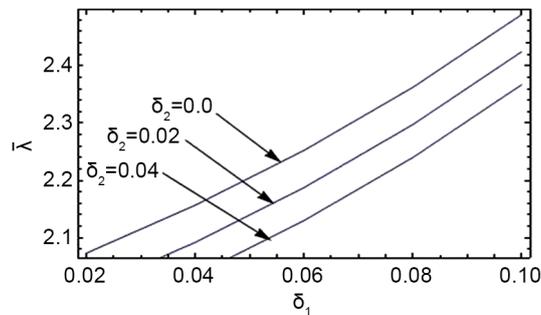


Figure 2. Variation of flow resistance $\bar{\lambda}$ with δ_1 for different δ_2 ($d_1 = d_2 = 0.2, L_1 = L_2 = 0.2, r = 0.8, q = 0.1, \bar{\alpha} = 1, \eta = 0.1, P = 0.1$).

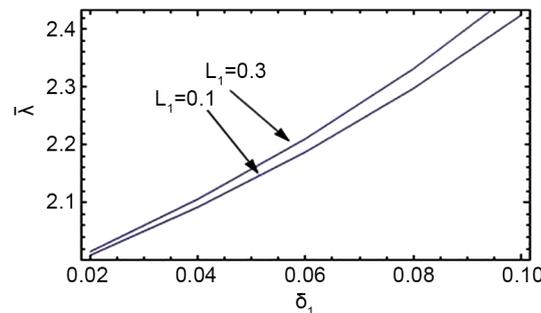


Figure 3. Variation of flow resistance $\bar{\lambda}$ with δ_1 for different L_1 ($d_1 = d_2 = 0.2, L_2 = 0.2, r = 0.8, q = 0.1, \bar{\alpha} = 1, \eta = 0.1, P = 0.1, \delta_2 = 0.02$).

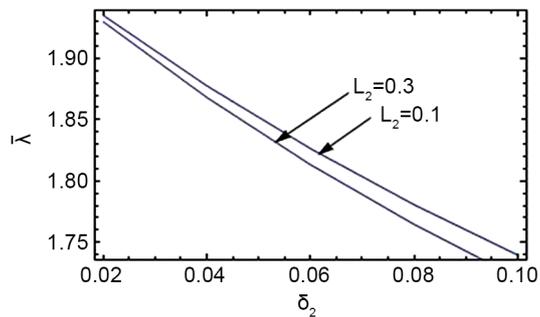


Figure 4. Variation of flow resistance $\bar{\lambda}$ with δ_2 for different L_2 ($d_1 = d_2 = 0.2, L_1 = 0.1, r = 0.8, q = 0.1, \bar{\alpha} = 1, \eta = 0.1, P = 0.1, \delta_1 = 0$).

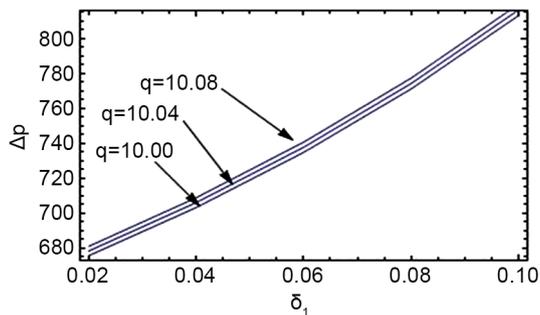


Figure 5. Variation of pressure drop Δp with δ_1 for different q ($d_1 = d_2 = 0.2, L_1 = L_2 = 0.2, r = 0.8, \bar{\alpha} = 1, \eta = 0.1, P = 0.1, \delta_2 = 0.01$).

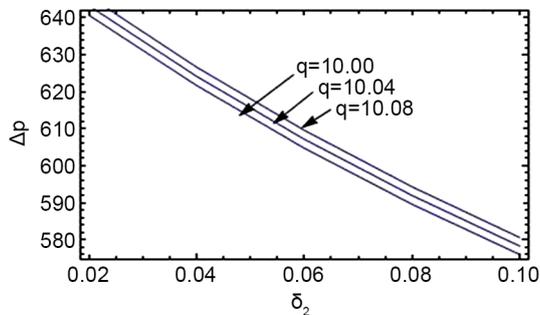


Figure 6. Variation of pressure drop Δp with δ_2 for different q ($d_1 = d_2 = 0.2, L_1 = L_2 = 0.2, r = 0.8, \bar{\alpha} = 1, \eta = 0.1, P = 0.1, \delta_2 = 0$).

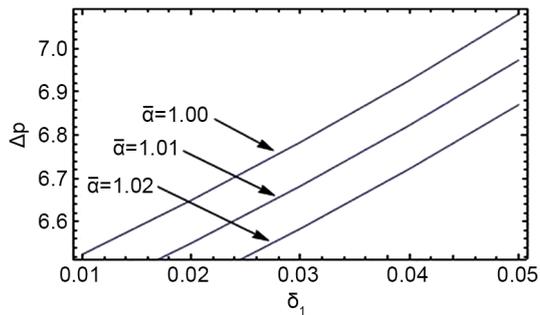


Figure 7. Variation of pressure drop Δp with δ_1 for different $\bar{\alpha}$ ($d_1 = d_2 = 0.2, L_1 = L_2 = 0.2, r = 0.8, q = 0.1, \eta = 0.1, P = 0.1, \delta_2 = 0.01$).

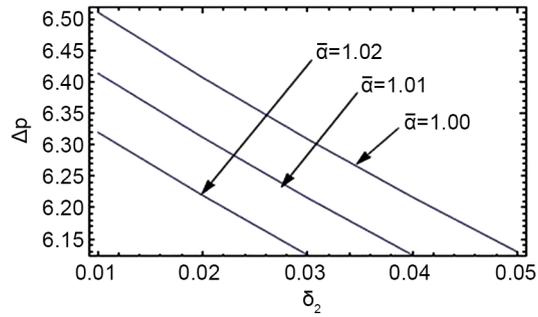


Figure 8. Variation of pressure drop Δp with δ_2 for different $\bar{\alpha}$ ($d_1 = d_2 = 0.2, L_1 = L_2 = 0.2, r = 0.8, q = 0.1, \eta = 0.1, P = 0.1, \delta_1 = 0$).

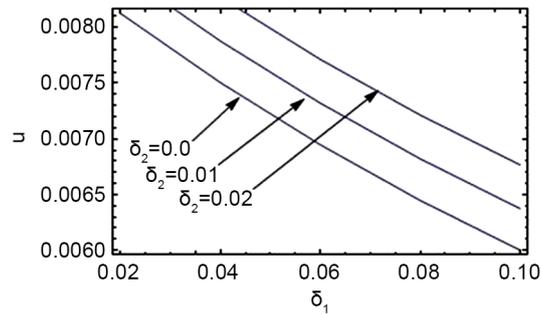


Figure 9. Variation of velocity u with δ_1 for different δ_2 ($d_1 = d_2 = 0.2, L_1 = L_2 = 0.2, r = 0.8, q = 0.1, \bar{\alpha} = 1, \eta = 1.7, P = 0.1$).

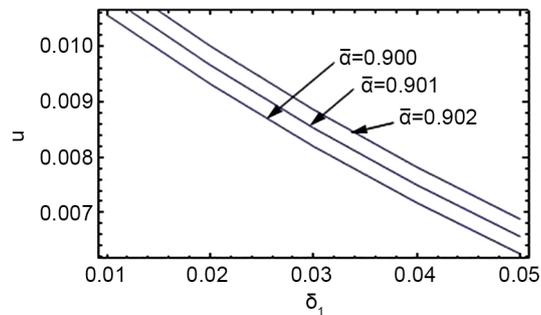


Figure 10. Variation of velocity u with δ_1 for different $\bar{\alpha}$ ($d_1 = d_2 = 0.2, L_1 = L_2 = 0.2, r = 0.8, q = 0.1, \bar{\alpha} = 1, \eta = 1.3, P = 0.1, \delta_2 = 0$).

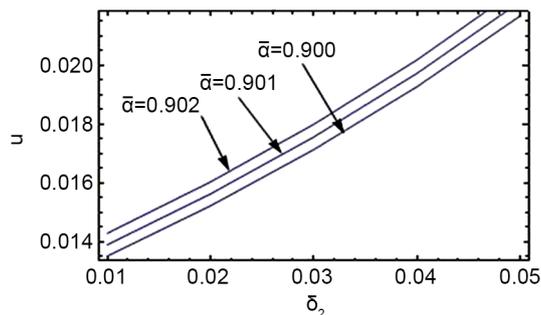


Figure 11. Variation of velocity u with δ_2 for different $\bar{\alpha}$ ($d_1 = d_2 = 0.2, L_1 = L_2 = 0.2, r = 0.8, q = 0.1, \bar{\alpha} = 1, \eta = 1.3, P = 0.1, \delta_1 = 0$).

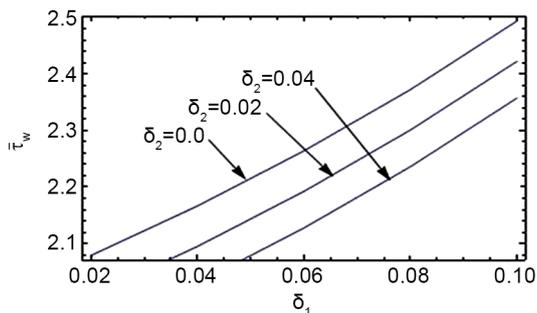


Figure 12. Variation of Shear stress $\bar{\tau}_w$ with δ_1 for different δ_2 ($d_1 = d_2 = 0.2, L_1 = L_2 = 0.2, \delta_2 = 0, r = 0.8, \mu = 0.2, q = 0.1, \bar{\alpha} = 1, \eta = 1.8$).

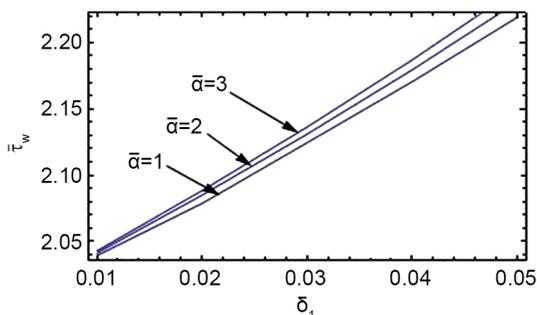


Figure 13. Variation of Shear stress $\bar{\tau}_w$ with δ_1 for different $\bar{\alpha}$ ($d_1 = d_2 = 0.2, L_1 = L_2 = 0.2, \delta_2 = 0, r = 0.8, \mu = 0.2, q = 0.1, \eta = 5$).

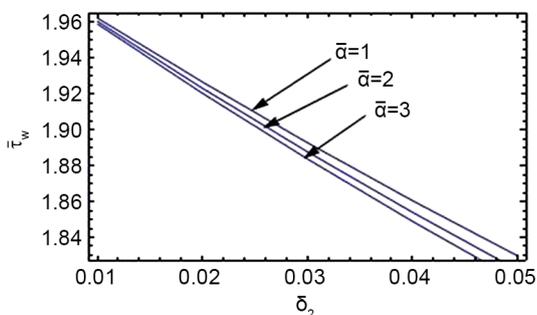


Figure 14. Variation of Shear stress $\bar{\tau}_w$ with δ_2 for different $\bar{\alpha}$ ($d_1 = d_2 = 0.2, L_1 = L_2 = 0.2, \delta_1 = 0, r = 0.8, \mu = 0.2, q = 0.1, \eta = 5$).

fluid parameter ($\bar{\alpha}$). It can also be observed that, the pressure drop decreases with height of post stenotic dilatation (δ_2) and couple stress fluid parameter ($\bar{\alpha}$) but increases with volumetric flow rate (q).

It is also noticed that velocity is decreases with height of the stenosis and increases with couple stress fluid parameter $\bar{\alpha}$ (Figure 9 & Figure 10). And velocity is increases with height of the post stenotic dilatation and couple stress fluid parameter (Figure 10 & Figure 11).

It is identified from the Figure 12 and Figure 13 that, the wall shear stress increases with height of the stenosis and couple stress fluid parameter but decreases with height of the post stenotic dilatation and couple stress fluid parameter (Figure 14).

4. Conclusion

A mathematical model for stenosis and post stenotic dilatation on the steady flow of couple stress fluid in a uniform tube has been presented. Solutions have been obtained for mild stenosis. It has been obtained that the resistance to the flow, pressure drop and shear stress increase with the height and length of the stenosis but decrease in the case of post stenotic dilatation. However, wall shear stress increases with height of the stenosis and couple stress parameter but decreases with post stenotic dilatation and couple stress fluid parameter.

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